

## Description

## Apparatus and method for protecting an electric machine

The present invention relates to a protective apparatus for protecting an electric machine against current overload. The present invention further relates to a corresponding method for protecting an electric machine.

Electric machines, in particular motors, can be operated temporarily with a current level above the rated or continuous current level. The reason for this is that overheating of the electric machine only occurs after a certain amount of time. The electric machines are therefore divided into certain  $\tau$  classes (CLASS or disconnection class). In each case the permitted multiple of the rated current and the period of time for which the electric machine can be operated at this increased current without overheating occurring are defined in these classes.

Until now mechanical overload relays have typically been used for motor protection. These overload relays are capable, by means of a bimetallic strip, of interrupting the power supply in the event of a limit current being exceeded, the time up to the interruption being a function of the current. The bimetallic element used for this purpose has been simulated in terms of its thermal properties in electronic overload devices for some time by means of software/firmware. In this case, a thermal variable, namely the thermal motor model (TMM), is used in order to set a thermal motor model curve as a function of a present current. The thermal motor model TMM can be represented as follows:

$$TMM = \left[ 1 - e^{-\frac{1}{\tau}} \right] \cdot \frac{I_{pres}}{I_{limit}}$$

Here,  $\tau$  corresponds to the time from the  $\tau$  classification,  $I_{pres}$  corresponds to the present current value,  $I_{limit}$  corresponds to a predetermined current limit value and  $t$  corresponds to the time. An overload device is triggered if  $TMM = 1 = 100\%$ . Assuming constant currents, the respective triggering time can thus be calculated if the machine is restarted, i.e. at  $TMM = 0$ .

Since this calculation in the firmware is complex owing to the need for precise time stamping, the function is simulated using the following recursive time formulation:

$$TMM_{n+1} = TMM_n - \frac{TMM_n}{\frac{\tau}{\Delta t}} + \frac{I_{pres}}{\frac{\tau}{\Delta t}}$$

The function values are calculated in the time frame  $\Delta t$ , and the respective value  $TMM_{n+1}$  is monitored with respect to a current-dependent disconnection threshold, a predetermined value.

With this implementation it is possible to realize a trigger for the overload function. In this case, triggering can be carried out by means of a disconnection command or direct current interruption.

A message/warning as to whether triggering will take place by the overload device is likewise possible with this technology. For this purpose, a test is carried out to establish whether the present current is greater than a predetermined limit current. In this case, a large, temporal, thermal reserve of the motor remains unconsidered in certain circumstances. A prediction as to when triggering of the overload device will probably take place has until now been made as follows: A PLC reads the present value of the TMM and the present current

from the electronic overload device in order to then make a prediction using the constants given. A necessary precondition is therefore that the overload device is capable of communication. One further disadvantage

when making the prediction is the fact that the present operating state of the overload relay (CLASS, imbalance, present current value, present limit value, ...) needs to be simulated. The prediction is therefore associated with a very high degree of complexity and can therefore not be carried out in real time. A further disadvantage thus results in that the user needs to simulate the model function in the user program of its controller. For this purpose, corresponding knowhow is required and considerable cycle loads result.

The object of the present invention is thus to propose an apparatus and a method for protecting electric machines with which it is possible to predict a temporal trigger reserve without a high degree of complexity.

This object is achieved according to the invention by a protective apparatus for protecting an electric machine against current overload having a current value provision device for the purpose of providing a present current value with which the electric machine is driven, a prediction device for the purpose of predicting an absolute or relative time value as a function of the present current value, and a utilization device for the purpose of utilizing the time value for generating a control signal.

In addition, the invention provides a method for protecting an electric machine against current overload by providing a present current value with which the electric machine is driven, predicting an absolute or relative time value as a function of the present current value, and generating a control signal using the time value and driving the electric machine using the control signal.

It is thus possible according to the invention to realize a temporal prediction, together with an evaluation of the dynamic, temporal

trigger reserve of an electronic overload function, in a device with overload functionality.

A present thermal variable with respect to the electric machine can be calculated in the prediction device on the basis of the present current value such that the thermal variable can be used as a basis for the prediction. The thermal variable, for example the thermal motor model TMM, is preferably calculated recursively in the prediction device. The present thermal variable is expediently used for dynamically calculating the time value for the prediction.

The prediction device and/or the utilization device can advantageously be parameterized. Any desired limit values and device properties can thus be prescribed and used in the prediction or utilization.

A disconnection signal or warning signal can be generated as a control signal in the utilization device. The prediction can thus be used to ensure that a desired control cycle with excessive current is not possible at all or that a warning is output when the control cycle is created or used to indicate that the control cycle has not completely run and a premature interruption has taken place.

It is therefore possible according to the invention for the calculation of the prediction of the temporal trigger reserve to be integrated in a device having an overload function. Owing to this integration, it is no longer necessary for the device having the overload function to be capable of communication.

In one specific embodiment, the temporal trigger reserve can be monitored by means of limit-value monitoring devices at a predictor limit value. The temporal trigger reserve and/or the result of the limit-value monitoring device can also be processed locally

or passed on to the controller (PLC) for processing purposes. The predictor limit value and the subsequent response may be parameterized or set, as already indicated.

The user can advantageously use the combination according to the invention of prediction and evaluation for the purpose of maintaining his processes. Furthermore, it is possible according to the invention for the user to utilize the maximum temporal, thermal reserve of the motor for his processes without any loss in the motor protection function or any risk to his processes.

One further advantage consists in the fact that the presently valid parameters/constants/operating circumstances (CLASS, currents, imbalance with respect to the phases) are always used in the calculation in real time since the calculation takes place in the overload device. This means, however, that the prediction and evaluation can take place in devices which are not capable of communication, the link between the prediction and evaluation - as already mentioned - taking place by means of parameters and adjusting elements.

The present invention will be explained in more detail with reference to the attached drawings, in which:

- figure 1 shows a block diagram of a motor protection device according to the invention;
- figure 2 shows a current waveform graph; and
- figure 3 shows a graph of the thermal variable TMM as a result of the current waveform shown in figure 2.

The exemplary embodiments described in more detail below represent preferred embodiments of the present invention.

Figure 1 illustrates, using a dashed line, a motor protection device 1. This motor protection device 1 has a motor protection unit 2 for current detection, current provision and TMM formation for the motor protection which obtains a present current value  $I_{pres}$  from a motor 7. In the event of overheating, the overload device 2 outputs a corresponding command to the motor controller 3 or directly interrupts the current supply to the driven motor.

The motor protection unit 2 provides a present thermal value  $TMM_{pres}$  to a prediction unit (TMP) 4, which is likewise integrated in the motor protection device 1. The prediction unit 4 forms a temporal prediction value, namely a temporal trigger reserve, from the thermal value  $TMM_{pres}$ , and provides this temporal prediction value to a comparator 5, which is connected to the prediction unit 4 and is likewise integrated in the motor protection device 1.

The comparator 5 can be parameterized via a parameterization unit 6 which is likewise integrated in the motor protection device 1. If possible, the motor protection unit 2 and the prediction unit 4 can also be parameterized via the parameterization unit 6. Corresponding connections are not illustrated in figure 1 for reasons of clarity.

It is established in the comparator 5 whether the temporal trigger reserve is greater or less than a parameterized limit value (predictor limit value). If the trigger reserve is less than the parameterized limit value (predictor limit value), a warning signal or control signal is output to the motor controller 3 such that either the user is warned that automatic shutdown is probably to be expected in the case of the desired driving,

or driving of the motor with the desired drive curve will not be permitted.

The motor controller 3 may also be integrated in the motor protection device 1.

In the example selected in figure 2, the motor is initially operated with a current which is below a standardized limit current window. This limit current window is defined as  $1.1 \dots 1.2 \times I_e$ . In this case,  $I_e$  corresponds to the set or rated current with which the motor can be operated continuously. After a certain amount of time, the current  $I_{pres}$  decreases (for example by means of a change in load) and then increases above the limit current window in which a limit current  $I_{limit}$  to be defined lies. This high current would lead to the motor being overheated for a long period of time.

In figure 3, the thermal variable  $T_{MM}$  is plotted which temporally corresponds to the current waveform shown in figure 2. The curve profile in the stepless sections is given by the exponential function described in the introduction to the description. Accordingly, the temperature of the motor increases in accordance with the mentioned exponential function once the motor has been switched on, but would not reach a specific trigger threshold, in this case 100%, since the current is below the limit current (cf. figure 2). When the current is subsequently reduced, the temperature also decreases again. If the current is then increased to a value above the limit current  $I_{limit}$ , the temperature increases continuously and reaches the trigger threshold  $T_{MM} = 100\%$ . At this point, the current to the motor is disconnected (cf. figure 2) such that the temperature of the motor also gradually decreases again (cf. figure 3).

In order to drive the motor or to fix current drive profiles, it is necessary to know the temporal trigger reserve at which  $T_{MM}$  reaches the threshold value 100%. It should thus be possible for a prediction to be made in real time of the temporal trigger reserve at any desired points in time. This should not only be based on the steady-state case in which the motor is continuously driven at a constant current, but also it should be possible for the dynamic variant to be

considered if the current changes in the course of driving.

One possible calculation method for determining the trigger reserve is based, for example, on the fact that a fictitious zero point of the  $e$  function is calculated. This zero point defines the point in time at which  $TMM = 0$  whilst taking into consideration the present  $TMM$  and the present current  $I_{pres}$ . With knowledge of the limit current  $I_{limit}$ , the  $\tau$  class and the imbalance information with respect to the phases which are present at that point in time, it is possible for a dynamic prediction to be made of the time taken before triggering, i.e. before the motor is disconnected. At any point in time, a present temporal prediction can be made on the basis of the fictitious zero point, as is indicated in figure 3 at the bottom by horizontal bars. In this case, the present  $TMM$  value and the present current can be taken into account with each updating.

According to the invention, the temporal prediction of the trigger reserve is linked with a user function. For example, the dynamic temporal prediction of the trigger reserve of an electronic overload function can thus be linked with an overload message or warning. As has already been mentioned, the user can be warned prior to using a drive profile which will probably lead to automatic shutdown of the motor. This undesired shutdown may have very disadvantageous consequences in certain processes.

The individual parameters for determining the trigger reserve can in this case be input by the parameterization unit 6 (cf. figure 1) using a corresponding input interface. In addition, a correspondingly obtained, possibly standardized prediction value of the temporal trigger reserve can be made available to a programmable logic controller (PLC) or another system for further processing purposes.

One specific exemplary embodiment of the present invention will be described below. Accordingly, a fan motor is necessarily required for cooling a production process, for example. Failure of the fan would lead to damage to the finish and would thus result in rejects. In accordance with the previous prior art, no mention is made before starting the finishing process as to whether the cooling can be maintained throughout the finishing process. According to the invention, the user then parameterizes the maximum process runtime as a predictor limit value. By appropriately adjusting the parameters, an instance of the required cooling time being undershot is defined as a process fault. Before the unmachined part is introduced into the finishing process, a check is carried out using the thermal memory predictor (TMP) and its limit-value monitoring device to establish whether the temporal thermal reserve is provided for the execution of the finishing process. It is thus possible for the motor and thus the entire process to be used in a more targeted manner. In particular, critical process sections can be safeguarded more effectively.